Refrigeration Cycle Experiment

Abstract:

The aim of this experiment is to construct the Vapour Compression Refrigeration Cycle on the Pressure-Enthalpy property diagram, and determine the Coefficient of Performance by Measuring the temperatures and pressures of the liquid and gas phases of the refrigerant at various locations. Also to identify the components of the mechanical refrigeration apparatus and the thermodynamic processes occurring in these components and analyse these processes in condenser, evaporator, compressor and throttle/expansion volvo

Methodology:

First the cooling water supply and mains supply was switched on to the unit. After that, the valves have been checked due Normal Operation which allowed vapour to be drawn from the evaporator by the compressor and for condensed liquid to return to the evaporator from the condenser. The third step was to let the water supply to the unit and to set the condenser cooling water flow-rate about 6 g/s. Then, the evaporator water flow has been sited to approximately 10 g/2 After that, the main switch of the compressor has tern upper on in order to supply energy. At that point, the reingerant flow rate has been adjusted for about 1 40, the unit has been allowed to run for approximately 10-15 minutes a stabilise for the surrouncing regin nment. From the cost, the vapourcompression tycle (the large P-h diagram) can be plotted.



Figure 1-pressure-enthalpy diagram for refrigerant solkane SES36

Theory and Analysis:

- 1. The refrigeration cycle has been plotted and it is dependent on the temperatures (t_5, t_6, t_7, t_8) and the absolute pressure of the evaporator and condenser.
- 2. The temperatures are given.
- 3. The absolute pressure has been calculated from the evaporator and condenser gauge relatively to the local atmospheric pressure.

Absolute pressure of condenser: $P_{abs} = P_{atms} + P_{gauge} = 1.026 + 0.45 = 1.476$ bar Absolute pressure of evaporator: $P_{abs} = P_{atms} - P_{vac} = 1.026 - 0.7 = 0.326$ bar

- The pressures had been converted to bars according to the graph given. 4.
- 5. two horizontal lines has been drawn which match the size of the plot and also the state of each process.
- Each temperature has been pointed in its own location and also to find the specific enthalpy. 6.
- 7. The rate of heat transfer from water to evaporator $\dot{Q}_e = \dot{m}_e C_P (t_2 t_1) = 7.75 \times 10^{-3} \frac{j}{c} \text{ or } w$. Direct substitution from the table
- 8. The rate of heat transfer from water to condenser $\dot{Q_c} = \dot{m_c}C_P(t_3 t_4) = 2.97 \times 10^{-4} \frac{j}{s} or w.$ Direct substitution from the table
- 9. Delivered pressure ratio= $\frac{Absolute \ pressure \ of \ condenser}{Absolute \ pressure \ of \ evaporator} = \frac{1.476}{0.326} = 4.52$
- 10. The coefficient of performance can be found through the temperatures (t_5, t_7, t_8) which the specific enthalpy can be found from.
- 11. $t_5 = h_5 = h_1$, $t_7 = h_7 = h_2$, $t_8 = h_8 = h_4 \therefore COP_{ref} = \frac{h_1 h_4}{h_2 h_1} = \frac{345 233}{390 345} = 2.5$
- 12. Isentropic efficiency can be determined from pointing a point from point (t_1) which is parallel to the blue line (hemope) it could be impossible but it can be approximated. This efficiency describes the Competence of the isentropic work which is the difference between the predicted point and point 1 e over the actual work done by the compressor.
 - 13. Isentropic efficiency $=\frac{h_7'-h_5}{h_7-h_5}=\frac{371-345}{390-345}=0.57$, $h_7=h_2$, $h_5=h_1$
 - 14. Power input to the refrigerant: $P_{comp} = \dot{m}_{ref}(h_2 h_1) = 45$, direct substitution from the table and graph.

Throttle valve The pressu gets reduced w = 0 n = constar

Data Evaporato Evaporato Evaporato Evaporato Evaporato Evaporato Condense Condense Condense Condense Condense Condense Compress Compress Refrigerar Throttle in Rate of He Rate of He Delivered Coefficien Isentropic Power inp

By using the pressure-enthalpy diagram shown for the refrigerant the values for (h) can be obtained, and the coefficient of performance of the refrigerant (COP_{ref}) can therefore be calculated to be 2.5. In general it is said that the reverse Carnot cycle is the most efficient refrigeration cycle operating between lower temperature zone, and higher temperature zone. However it is not a suitable model for refrigeration cycles since processes 2-3 and 4-1 are not practical. In process 2-3 the condenser must be able to handle refrigerants in two phases (gas and liquid). And process 4-1 involves the expansion of a high moisture-content refrigerant in a turbine.also, it appear that The refrigerant evaporates at a lower temperature and low pressure drawing in heat, The refrigerant condenses at a higher temperature and higher pressure radiating heat, The cycle is not the most practical because it involves condensing refrigerants of 2 phases in one component, It also involves expansion of the refrigerant in a turbine which can lead to damage.







able 1 – investigation of system performance

	value
Gauge Pressure, Peg (kN/m2)	-70
Absolute Pressure, Pea (bar)	0.326
Inlet Water Temperature, t1 (°C)	23.3
Outlet Water Temperature, t2 (°C)	20.2
Refrigerant Temperature, t5 (°C)	8.5
water flow-rate, me (g/s)	10
Gauge Pressure, Pcg (kN/m2)	45
Absolute Pressure, Pca (par)	1.476
Inlet Water Temperature, t4 (°C)	23.7
Outlet Water Temperature, t3 (°C)	30.8
Refrigerant Temperature t6 (°C)	38.7
water flow-rate, mc (g/s)	6
r Discharge Temp, t7 (°C)	59.7
r Power Input, Pmech (Watts)	170
: mass flowrate mref (g/s)	1.0
et temperature t8 (°C)	31.5
at Transfer from Water Qe (w)	7.7*10^-3
at Transfer from Water Qc (w)	2.9*10^-4
Pressure Ratio	4.52
of Performance (COP)	2.5
efficiency of compressor	0.57
it to the refrigerant (W)	45

Reference:

Group members:

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