

# Outline

- FM Demodulation Techniques

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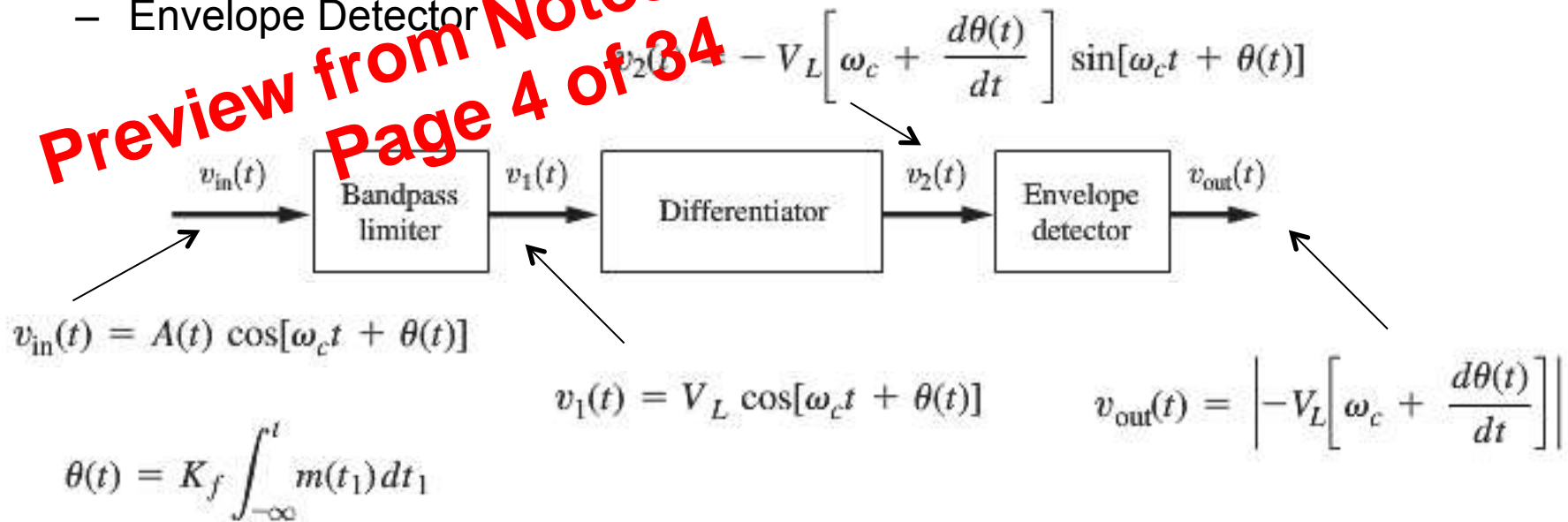
# FM Demodulator Classification

- Coherent & Non-coherent
  - A coherent detector has **two inputs**—one for a reference signal, such as the synchronized oscillator signal, and one for the modulated signal that is to be demodulated.
  - A noncoherent detector has only **one input**, namely, the modulated signal port.
  - **Example:** The envelope detector is an example of a noncoherent detector.
- Demodulator Classification
  - Frequency Discrimination
    - Noncoherent demodulator
    - FM→AM→ED→m(t)
  - Phase Shift Discrimination
    - Noncoherent demodulator
    - FM→PM→m(t)
  - Phase-Locked Loop (PLL) Detector
    - Coherent demodulator
    - Superior performance; complex and expensive

Let's look at each!

# Frequency Discrimination

- Components
  - Bandpass Limiter: Consists of **Hard Limiter** & **BP Filter**
  - Discriminator (frequency discriminator gain:  $K_{FD}$  V/rad - assume unity)
  - Envelope Detector



Note:  $D_f = K_f$   
 Freq. deviation sensitivity

THE OUTPUT WILL BE:

$$v_{out}(t) = V_L \left[ \omega_c + \frac{d\theta(t)}{dt} \right]$$

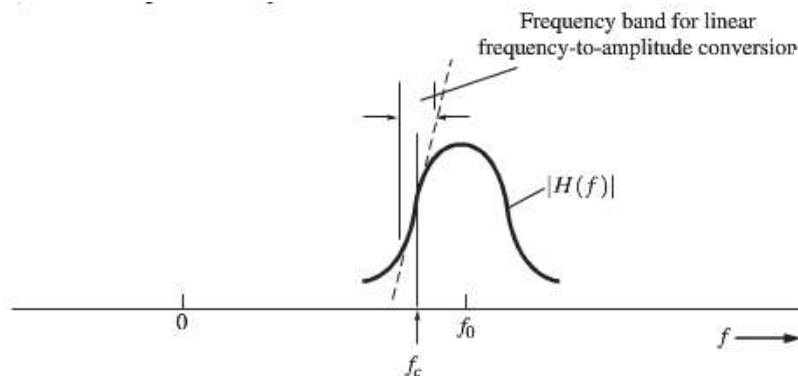
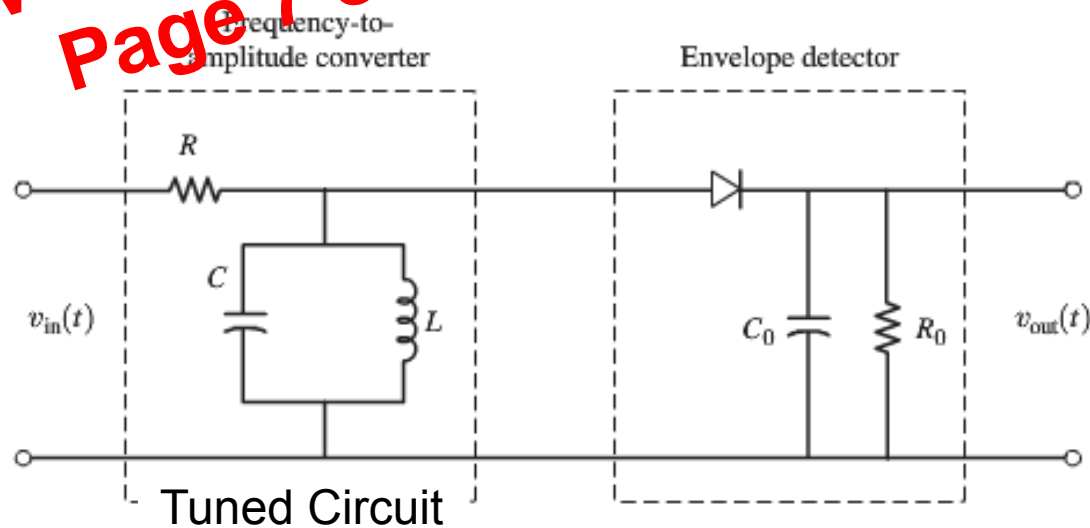
$$v_{out}(t) = V_L \omega_c + V_L K_f m(t)$$

DC Component can be blocked  
 by an AC coupled circuit

# Frequency Discrimination – Slope Detector

- In practice the differentiator can be approximated by a **slope detector** that has a linear frequency-to-amplitude transfer characteristic over the bandwidth BW – One drawback is that it is **narrow band**

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$$|H_{\text{slope\_det}}(f)| = \begin{cases} 2\pi K_{FD} \left| f - \left( f_c - \frac{B_T}{2} \right) \right| & f_c - \frac{B_T}{2} \leq f \leq f_c + \frac{B_T}{2} \\ 2\pi K_{FD} \left| f + \left( f_c - \frac{B_T}{2} \right) \right| & -f_c - \frac{B_T}{2} \leq f \leq -f_c + \frac{B_T}{2} \\ 0, & \text{otherwise} \end{cases}$$

BT is Carson's BW

# Analog Loop Filter – First Order

How does the control voltage  $v_2(t)$  change if the frequency of the input signal changes?

$$\omega_{in}(t) = \omega_c + \Delta\omega \cdot u(t) \rightarrow \theta_i(t) = \Delta\omega \cdot t$$

$$\Theta_{in}(f) = \Delta\omega / (j\omega)^2; s = j\omega$$

$$\Theta_i(s) = \Delta\omega / (s)^2$$

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$$v_1(t) = K_d \cdot v_o(t) \cdot v_{in}(t)$$

$$V_1(f) = K_d \cdot \Theta_e(f)$$

